

FREJUS HIGHWAY TUNNEL

Presented by Magali SCHIVRE , Systra



Client



Project Manager



Constructor



OUTLINE

- 1. General Overview**
- 2. Specific geological context**
- 3. Specific design of a hard rock single shield TBM suited for high deformable rocks**
- 4. Knowledge acquired during the construction**
- 5. Conclusions**



1.



GENERAL OVERVIEW

SYSTRA

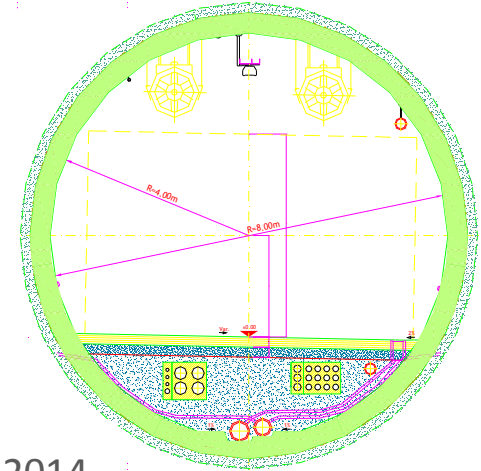
A second tube for the Frejus Highway tunnel

Improve the level of safety with a second tube :

- $L \approx 13\text{km}$, $\varnothing_{\text{utile inside}} 8,00\text{m}$ (8,20m inside),
- 34 by-pass = “safe area”
- 5 by-pass for vehicles

Current progression

- Work started in December 2009
- TBM started on 5th July 2011, at PM 654 - Ended on the 17th November 2014
- End of civil works in 2017



PROJECT COSTS & ACTORS

Total Project Cost is about **400 M€**, shared between France & Italy (GC 250M€, equipment 50M€, others 100M€)

Main ACTORS:

- 2 Clients: SFTRF, SITAF
- 1 Operator: GEF



- Project Manager: I3S (SYSTRA mandatory, SWS et SEA)



- Contractor Joint Venture :

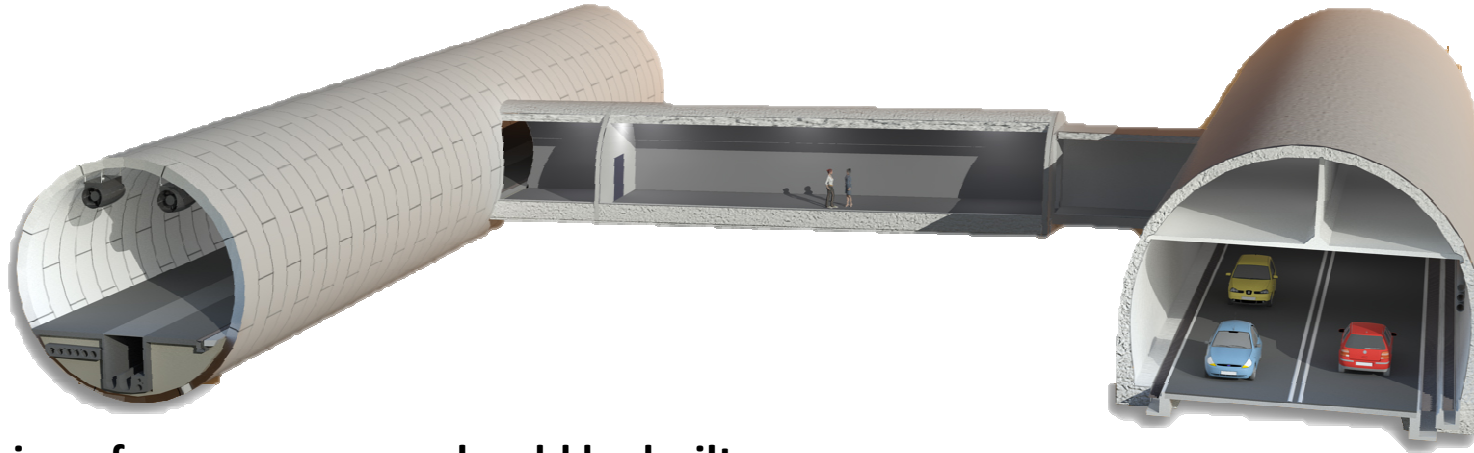
Lot 1 (French side): RAZEL - BILFINGER



Lot 2 (Italian side): ITINERA - RAZEL



SPECIFIC CONSTRAINTS



The opening of cross-passages should be built near the back of the machine, and activated for operation progressively

- Opening of the last by-pass at a maximum distance of **1000m** from the TBM
- The by-pass must be operational not later than **4 months** after the TBM excavation

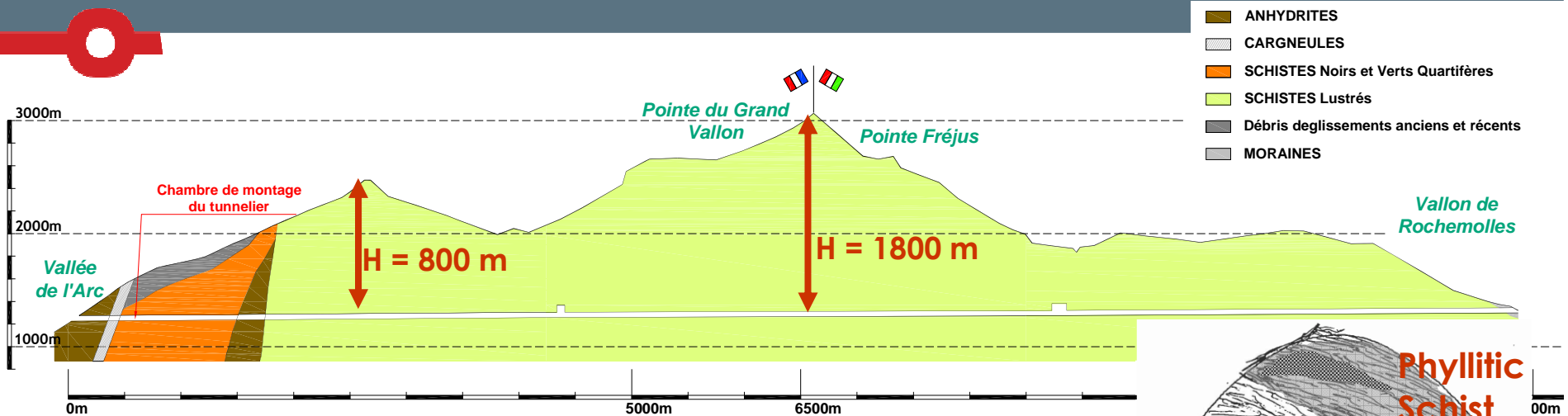




SPECIFIC GEOLOGICAL CONTEXT

SYSTRA

GEOLOGICAL & GEOMECHANICAL CONTEXT

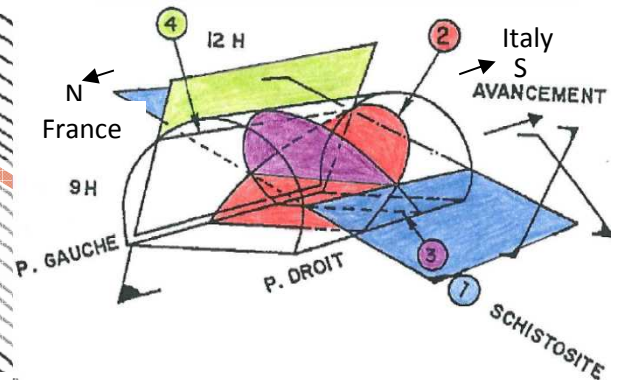
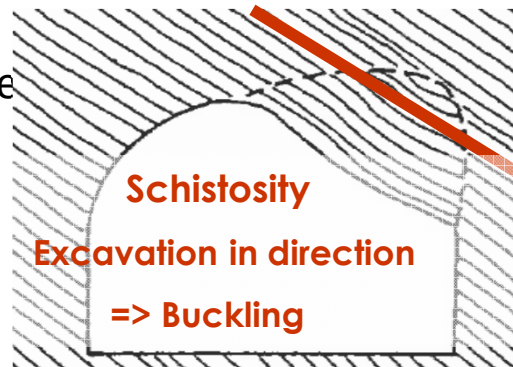


High overburden from 800 to 1800 m

From Triassic series (Anhydrite, Chert, Quartz, Black and Green Schist) & through the calc-schist formation (*schistes lustrés*)

The Calc-schist rock mass is characterized

- Anisotropy of composition
- Anisotropy due to schistosity
- Anisotropy of stress field $\sigma_H = 1.2 \text{ to } 1.4 \sigma_V$



FREJUS HIGHWAY TUNNEL BUILT FROM 1974 TO 1979

Highway tunnel // new gallery (Inter-axis = 50 m)

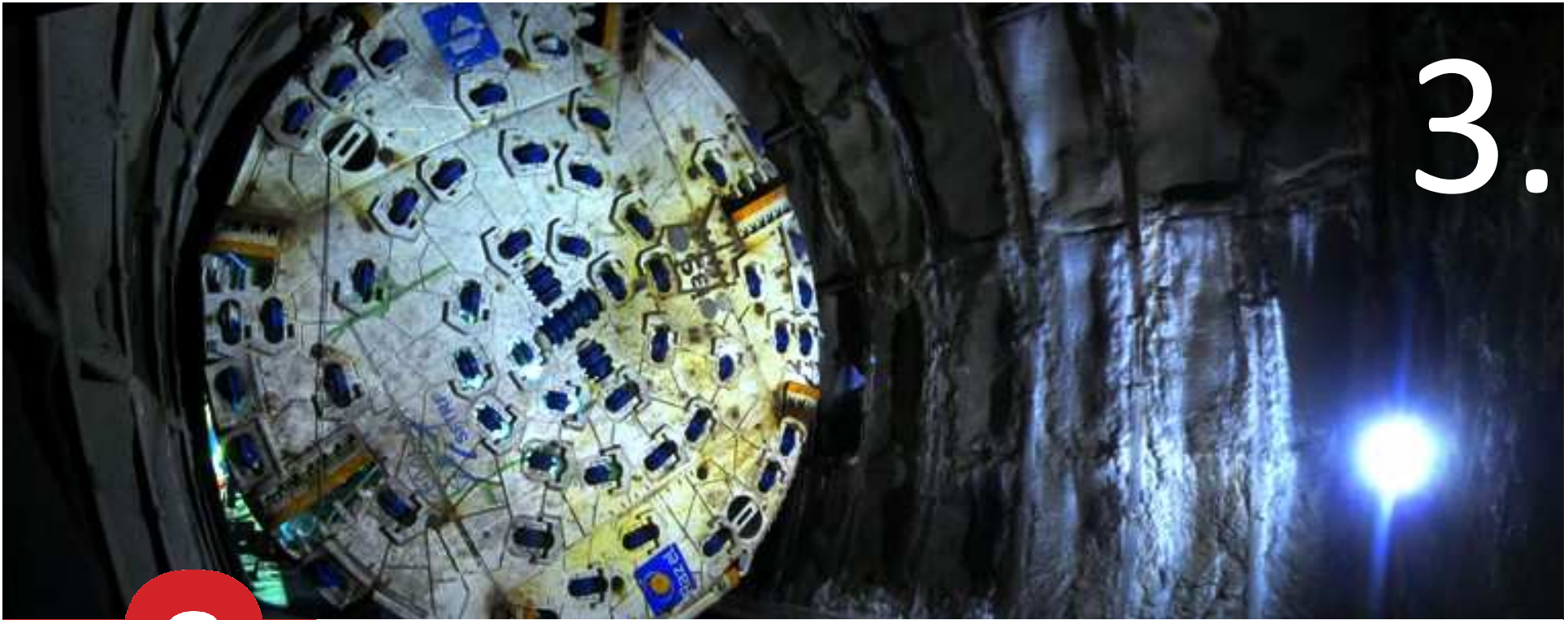
Issues started at the beginning of the Calc-schist formation

Drill & Blast methods, flexible support (bolts density : $1,2 \text{ u/m}^2$)

- Convergence up to 45cm (Schist buckling + Squeezing phenomena)
- Development of a plastic zone up to 10m around the excavation
- High stress level ; Very high loads on the support, Rupture & Shearing of the bolts



3.



Design of a Single Shield TBM *suited for highly deformable rocks*

SYSTRA

An adaptable TBM with the following requirements

A hard rock single shield TBM, suited for highly deformable rocks:

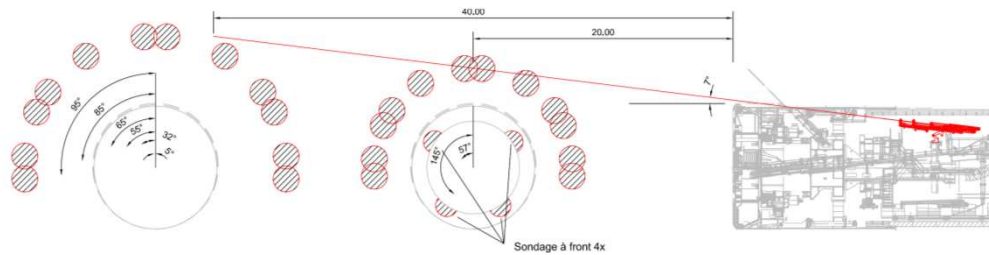
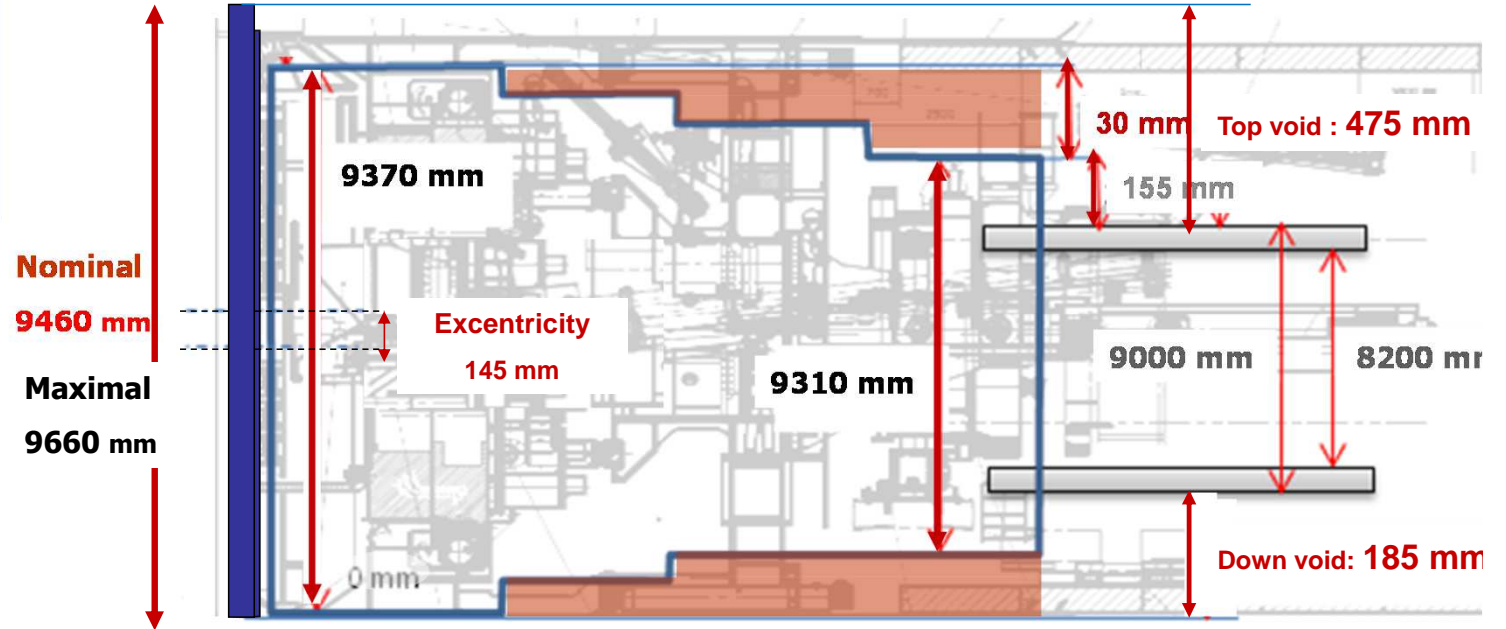
- Short single shield ***Length = 11.20 m ; Cutterhead diameter 9,46 m***
- High breakaway Thrust ***Total Breakaway Thrust 106 160 kN ; Breakaway Torque 21 289 kNm***
- Reinforced Shield

To allow some convergences and to limit the extension of the plastic zone

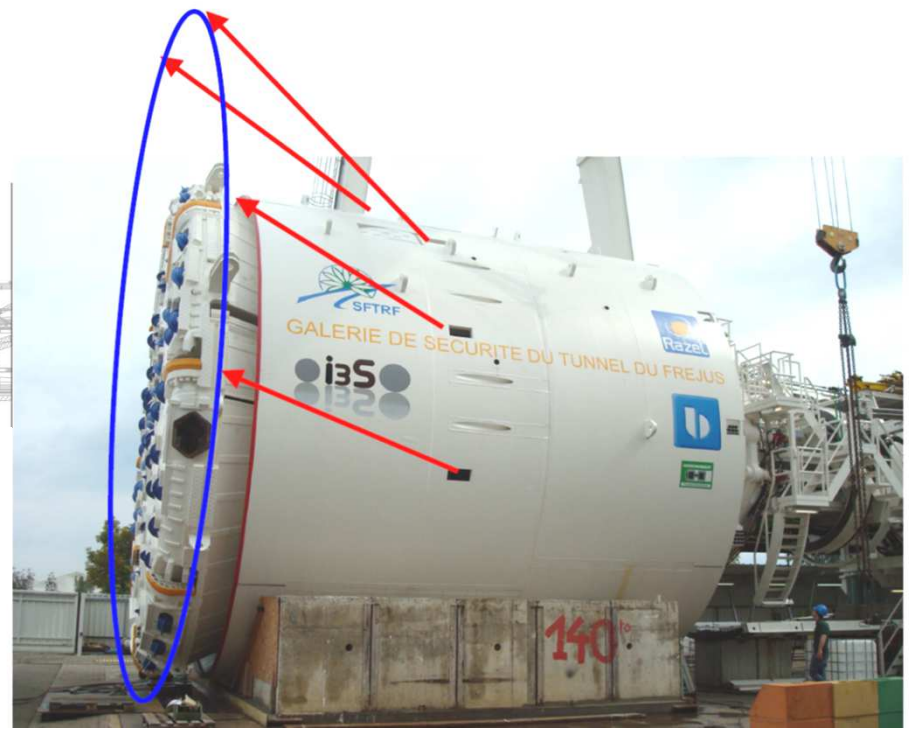
- High Shield conicity ***60 mm on diameter***
- Big annular void
- Possibility to increase the boring diameter
- Possibility of **bolting** from the shield
- Possibility of ***probe drilling survey*** at the front



An adaptable



*12 openings on the shield
 4 position in the front, 2
 opening in the cutterhead*

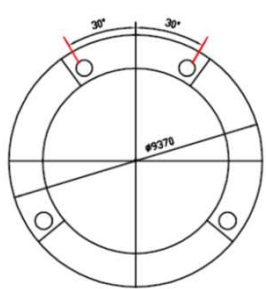




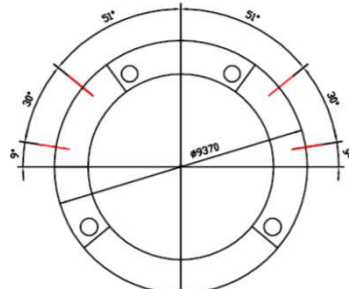
TBM EQUIPMENT – Gap around the shield measuring



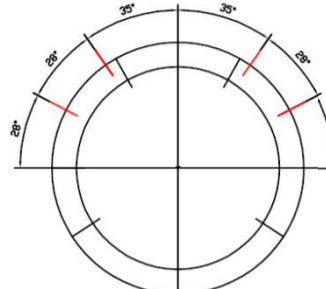
10 hydraulic jacks to measure the gap around the shield



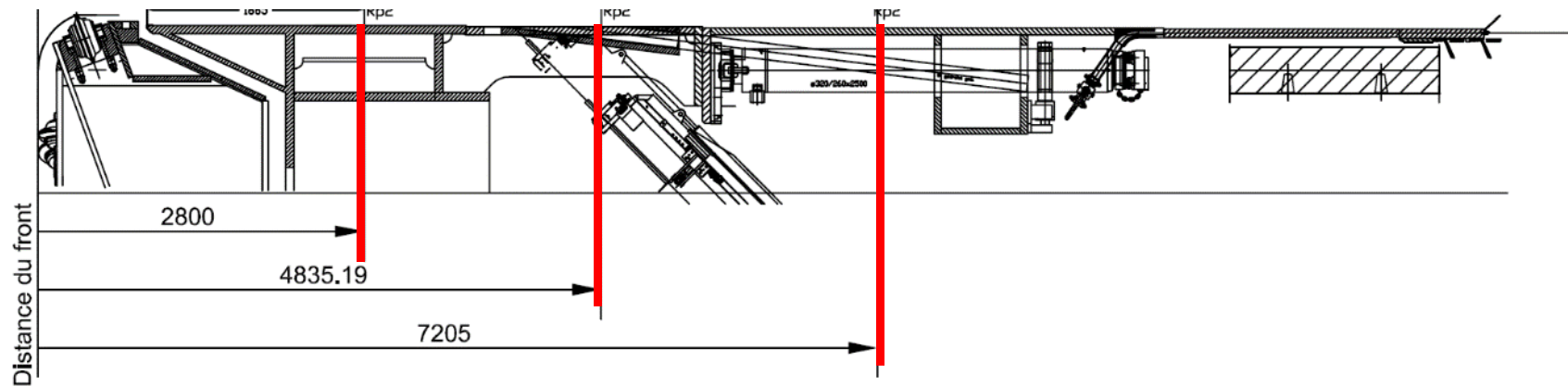
2



4



4



SEGMENT LINING

Adapted dimensioning of the segments lining and their framework Universal Ring

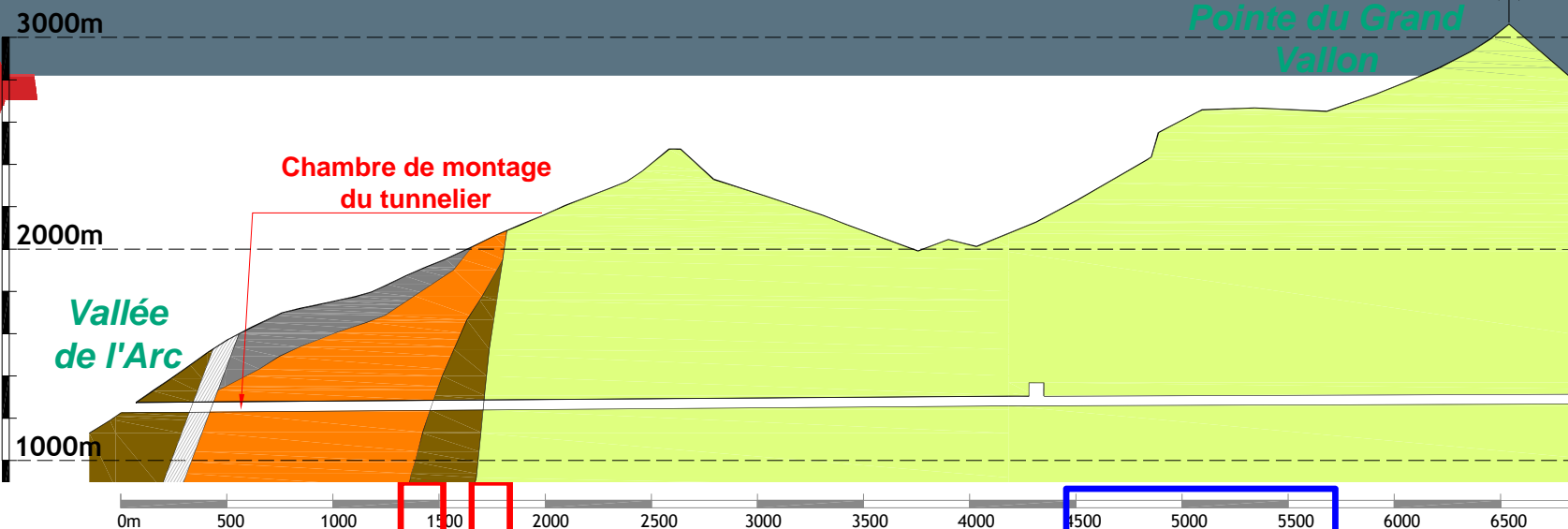
Ring Division:	6+1
Segment Length:	1800 mm
Segment Inner Diameter:	8200 mm
Segment Outer Diameter:	9000 mm

Two types of segments :

- *Type 1: C35/45 - 80 kg/m³ steel ratio - 2 SOF-Clips*
- *Type 2: C35/45 - 125 kg/m³ steel ratio - 2 x2 SOF-Clips*



INITIAL MODEL OF Advancement Plan for the TBM



Géologie	Schiste noirs et verts	Amphibolites	Calschistes				
Couverture	H < 800m		H = 1223m	H < 1000m	H = 1200m	H = 1404m	Forte couverture
Accident géologique répertorié		Faille?					
Convergences	Zone non convergente	Fortes convergences	Convergences modérées	Fortes convergences	Convergences modérées		
Bouclier							
Poussée théorique sur bouclier	5000-1000kN	< 5000 kN	1000-3500kN	10000-15000 kN	35000/40000kN	5000/15000kN	20000kN à 35000/40000kN
Nature des efforts sur le bouclier	Flambement potentiel	Flambement/Convergences	Possibilités de ruptures limitées à ruptures étendues		Convergences	Flambement	Etat de contraintes élevées
Surcoupe	Nominale 90/275 190/375 290/475						
Boulonnage radial		Boulonnage radial			Boulonnage radial		
Revêtement							
Charges sur l'anneau	260 à 490 kPa		325 - 680 kPa à 480 kPa - 1100 kPa		650 - 1200 kPa		
Armature de l'anneau	Type 1 Type 2						
Anneaux instrumentés							
Bourrage compressible							
Zones de vigilance		0°	1°	2°	3°	4°	

1st Zone

2nd Zone

4.



Knowledge acquired during the construction

SYSTRA

A learning method, utilizing anticipation, retroanalysis

*As for conventional method, a team of engineers was dedicated to the **follow up** excavation parameters and able to decide to set up adaptation on TBM, taking into account the industrial process of TBM advancement*

Actions implemented to follow the construction and anticipate problems :

- **Follow up of the construction with Systematic analysis , with Threshold values calibration**



- **Set up TBM adaptations or countermeasures**

Follow up of the construction & Monitoring

TBM Parameters follow up

Geological investigation:

- Systematic probe drilling survey
- Radial Boreholes
- Analysis of the annular void (openings, endoscope)

LINING Follow up :

- Strains gauges in the lining
- In-situ stress measure
- Deformation measures

Date :		16/11/2011		Anneaux		525 à 531				
Paramètres étudiés	U	Seuil de vigilance		Seuil d'alerte		16/11/2011			15/11/2011	Comparaison J / J-1
		mini	max	mini	max	Valeur mini du jour J	Valeur maxi du jour J	Moyenne de J	Moyenne de J-1	% variation
Verin R1	mm	<>	80 200	<>	50 300	109	149	129	106	↑ 21%
Verin R2	mm	<>	80 200	<>	50 300	35	147	107	22	↑ 379%
Verin R3	mm	<>	80 200	<>	50 300	73	140	119	119	→ 0%
Verin R4	mm	<>	80 200	<>	50 300	73	129	110	111	→ -1%
Verin R5	mm	<>	80 200	<>	50 300	101	144	118	121	→ -3%
Verin L1	mm	<>	80 200	<>	50 300	137	188	165	159	→ 4%
Verin L2	mm	<>	80 200	<>	50 300	159	179	169	160	→ 6%
Verin L3	mm	<>	80 200	<>	50 300	152	187	171	161	→ 6%
Verin L4	mm	<>	80 200	<>	50 300	159	175	167	158	→ 5%
Verin L5	mm	<>	80 200	<>	50 300	151	164	159	152	→ 4%
Force de poussée totale	KN	>	30 000	>	35 000	19 000	29 900	23 986	25 664	→ -7%
Force de frottement	kN	>	10 000	>	12 500	10 000	13 800	11 743	14 927	↓ -21%
Force de poussée sur le terrain	kN	<	10 000	<	8 000	9 800	15 800	12 400	11 082	↑ 12%
Poids de marinage	T	>	210	>	220	185	203	193	203	→ -5%
Vitesse de creusement	mm/min	>	60	>	75	64	84	77	71	→ 8%

<	Seuil mini
>	Seuil maxi

Alerte
Vigilance
OK

Follow up of the construction & Monitoring

○ TBM Parameters follow up

○ Geological investigation:

- Systematic probe drilling survey
- Radial Boreholes
- Analysis of the annular void (openings, endoscope)

○ LINING Follow up :

- Strains gauges in the lining
- In-situ stress measure
- Deformation measures



Carottage radial



Annular void



Shield windows

Follow up of the construction & Monitoring

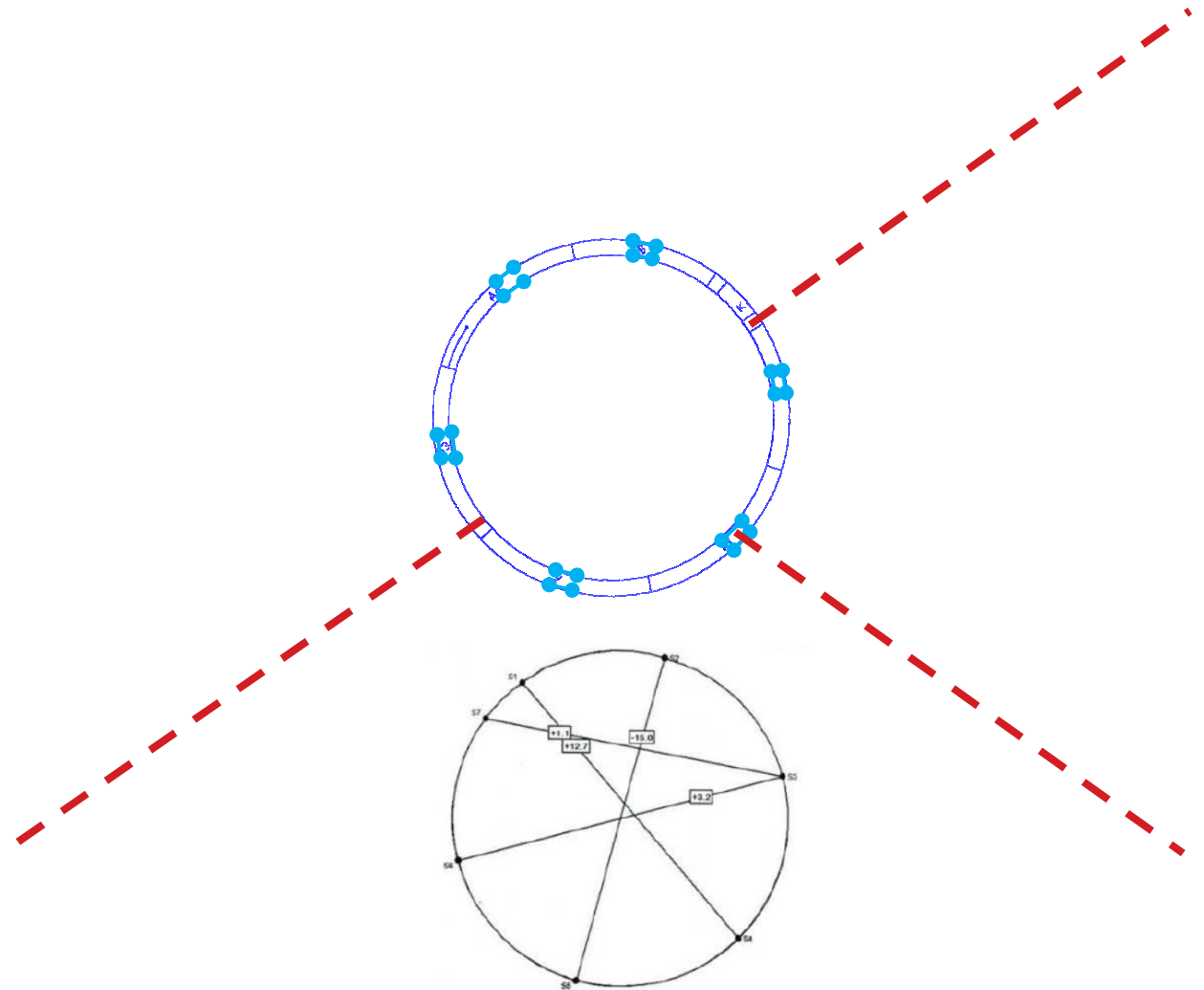
○ TBM Parameters follow up

○ Geological investigation:

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○ LINING Follow up :

- Strains gauges in the lining
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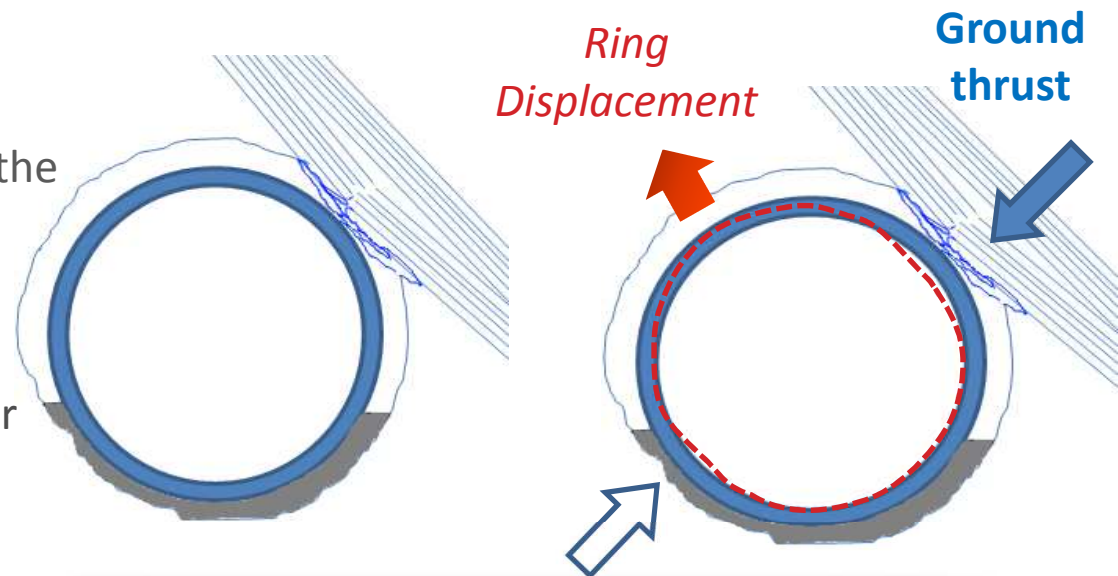


Buckling phenomena - First zone



Observed behaviour :

- Buckling caused rock contact against the shield and the segment lining, on the right side of the gallery
- Issues to fill the annular void
- A very dense schistosity, RQD =0, poor rock mass quality



Consequences:

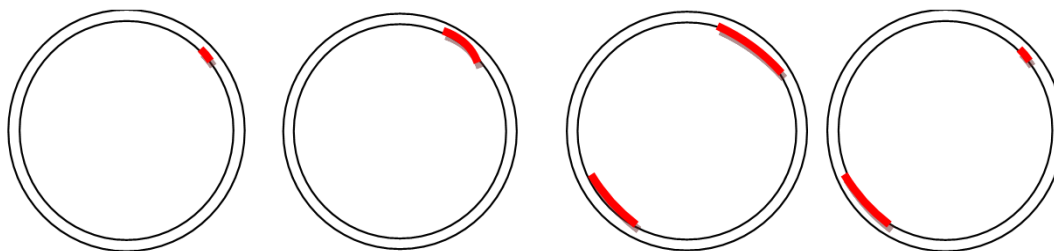
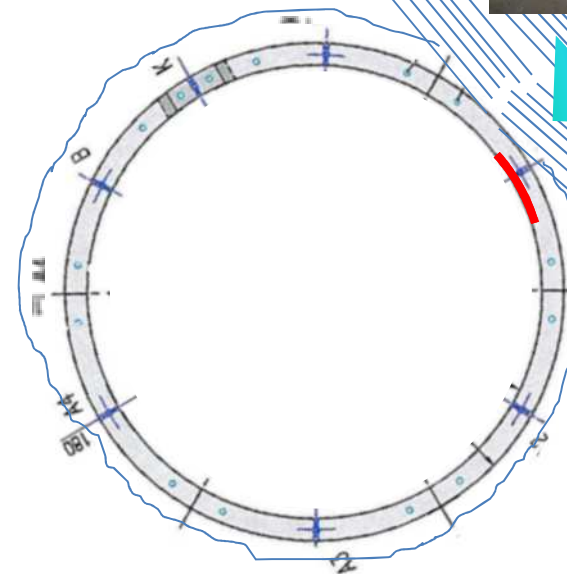
- Very localized load (L=2m) => asymmetric loading
- Lack of abutment leads to ring displacement
- Significant cracks on segment lining



Buckling phenomena, around PM 1500

Consequences of buckling :

- Occurrence of cracks on segment lining (1mm to 2mm)



- Odd rings: **opening joints + offset**
- Even rings: **cracks (1mm to 2mm)**

Counter-measures during excavation

First zone of convergences (PM 1 180 – 2 980)

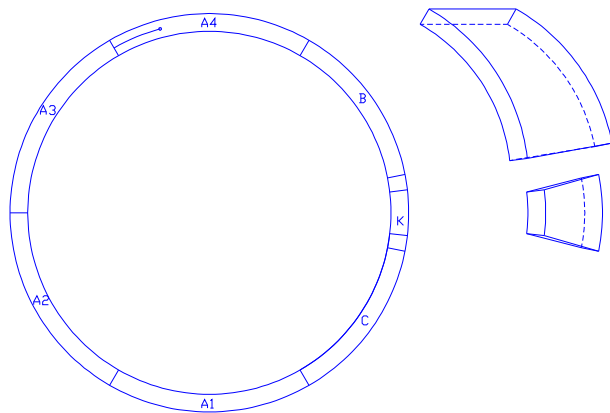
- Non-expected zone
- Very high Thrust(50 000kN)
- Low values of the hydraulic jacks on right side

Counter-Measures implemented

Second Type of segments

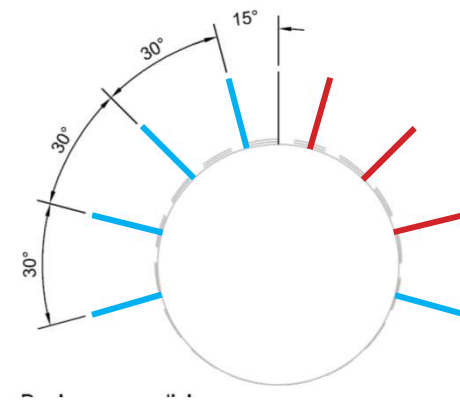
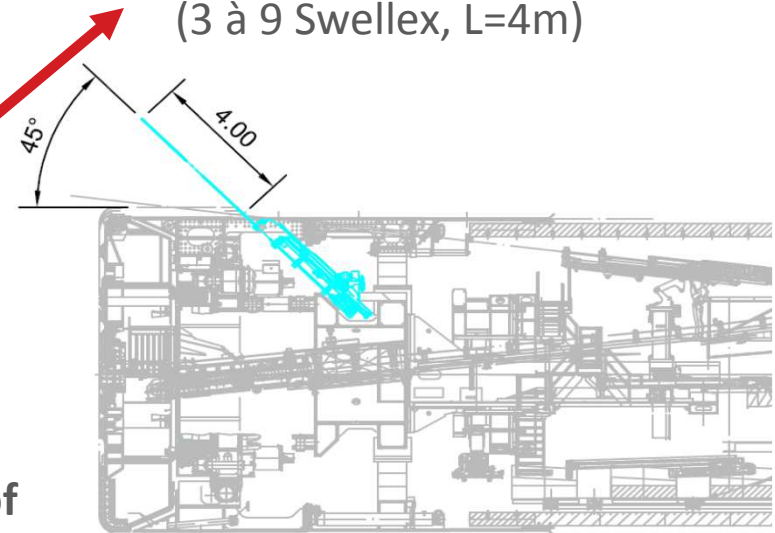
(125 kg/m³ steel ratio)

2 x2 SOF-Clips



Increase the diameter of excavation
(190mm)

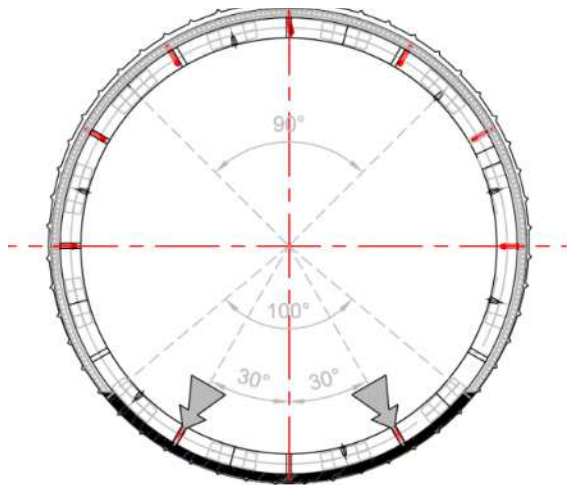
Radial rockbolts
(3 à 9 Swellex, L=4m)



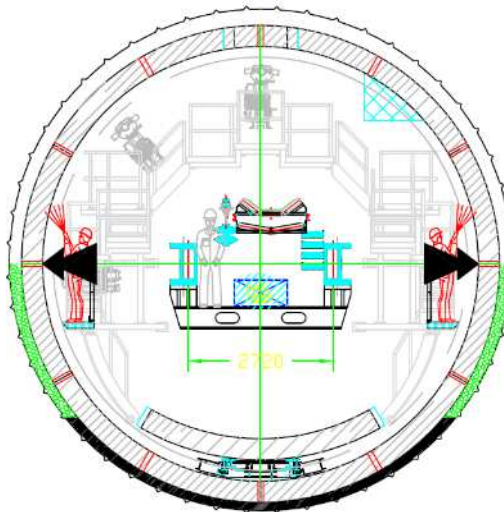
Improvement of the annular void filling

Initial procedure to fill the annular void

Mortar at the invert
During TBM progress

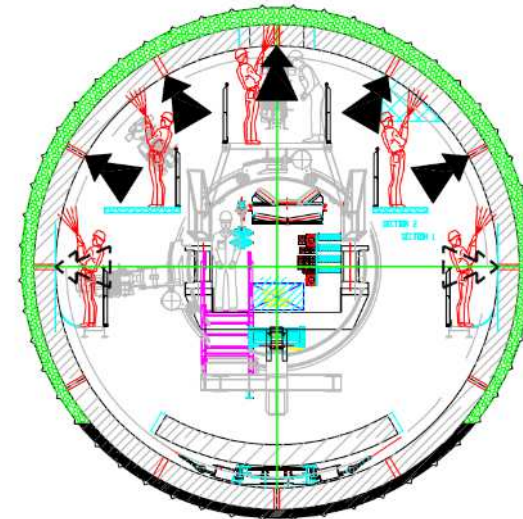


Ring N-2
Filling with pea gravel



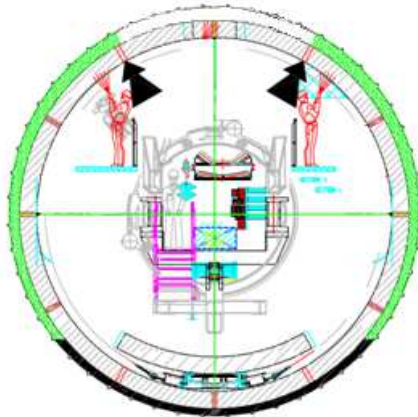
Ring N-5 to N-7
Filling with pea gravel

3h et 9h; 2h et 10h; 1h et 11h; 12h



Improvement of the annular void filling

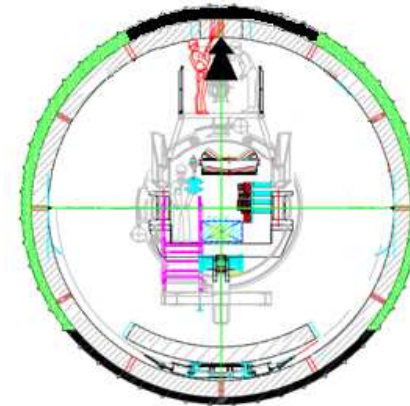
Ring N-2
Filling with pea gravel



Filling with pea gravel



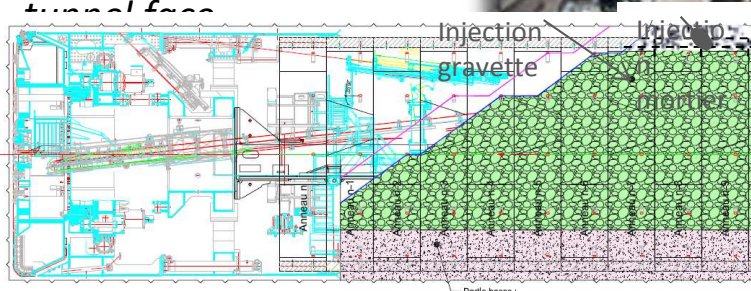
Ring N-5 to N-7
Filling with mortar



Filling with mortar at the crown



Issues to fill the void with mortar from the tailskin because of the important shield conicity => the mortar flows towards the tunnel face



Design & construction of New type of segment T3

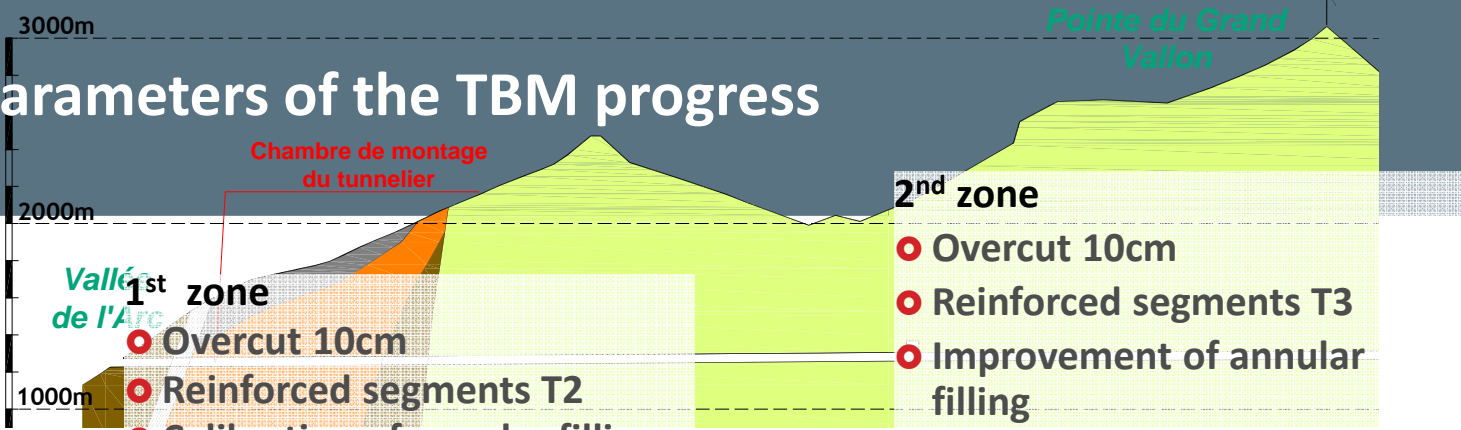
Augmentation of the steel ratio of the segments in order to avoid the cracking phenomena

A third type of segments is designed :

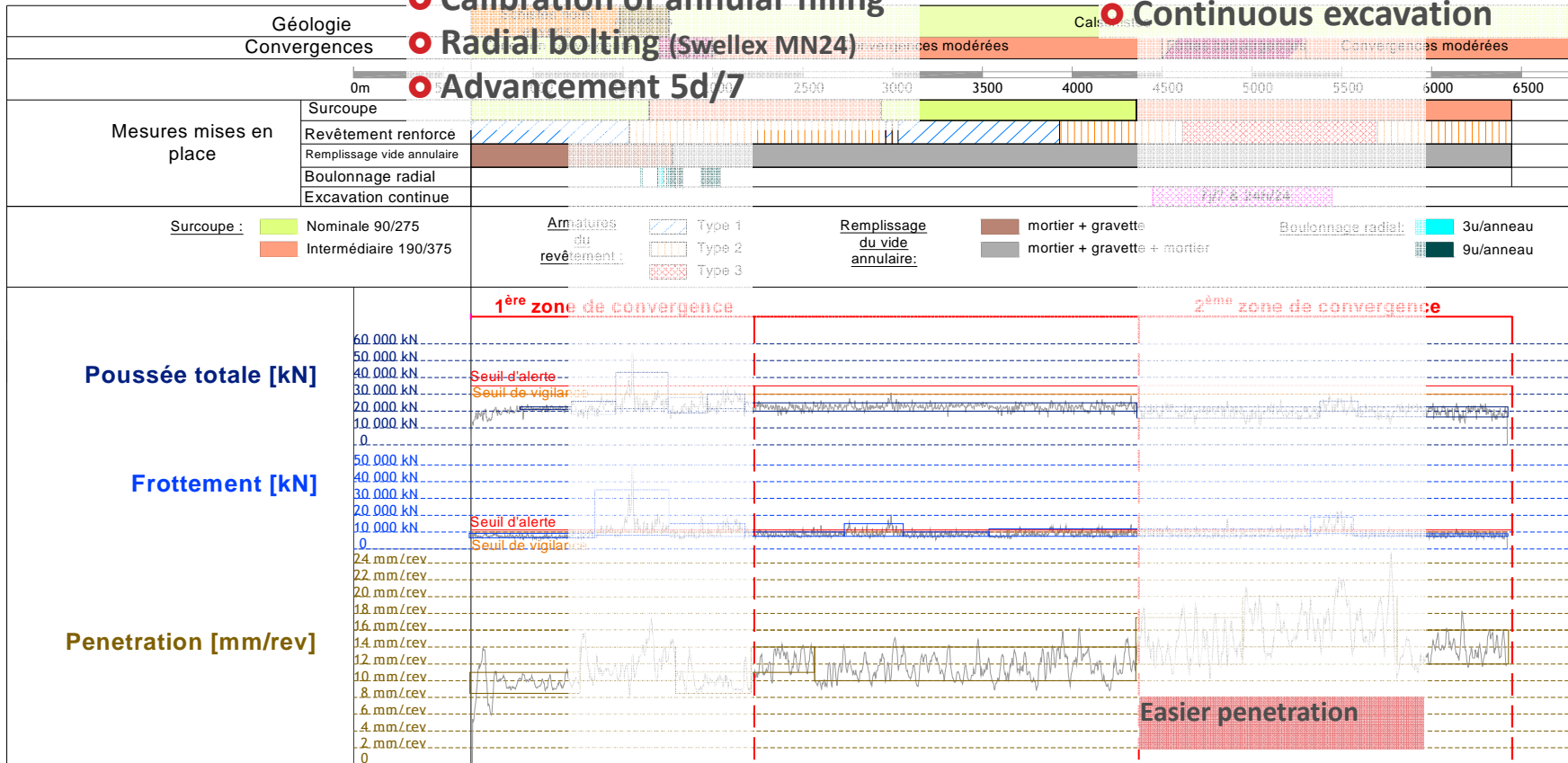
- Type 3: C35/45 - 285 kg/m³ steel ratio
- 2 x2 SOF-Clips with reinforced web

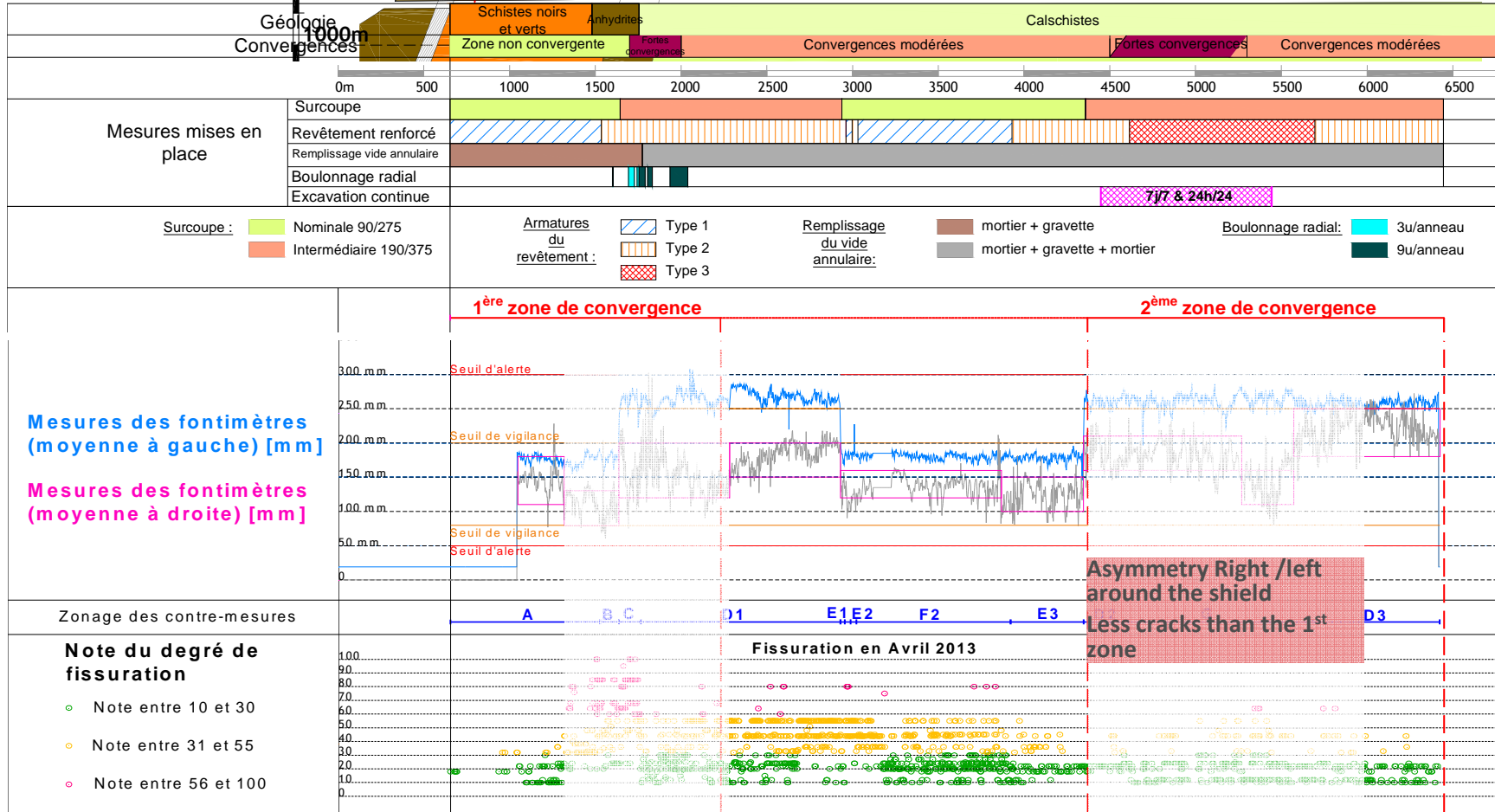
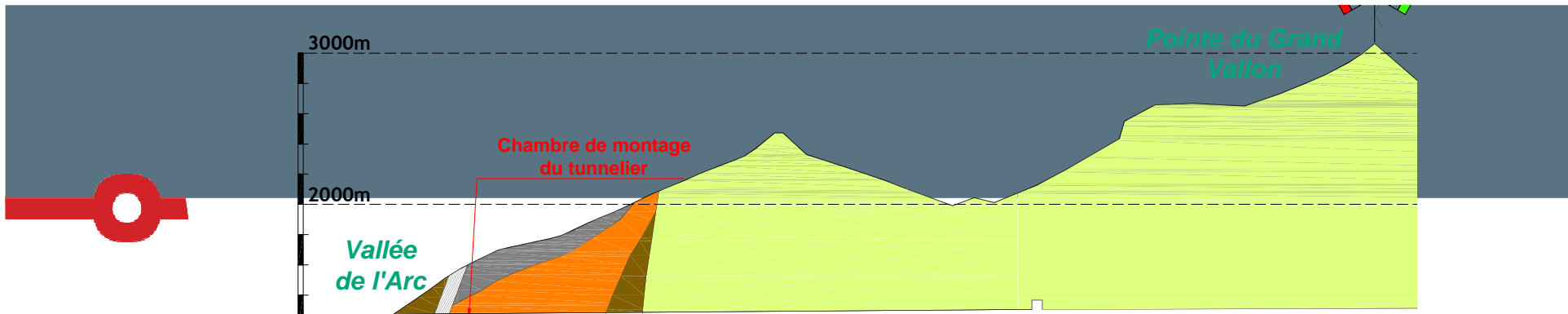


Drilling parameters of the TBM progress



- 1st zone**
- Overcut 10cm
 - Reinforced segments T2
 - Calibration of annular filling
 - Radial bolting (Swellex MN24)
 - Advancement 5d/7
- 2nd zone**
- Overcut 10cm
 - Reinforced segments T3
 - Improvement of annular filling
 - Continuous excavation







5.



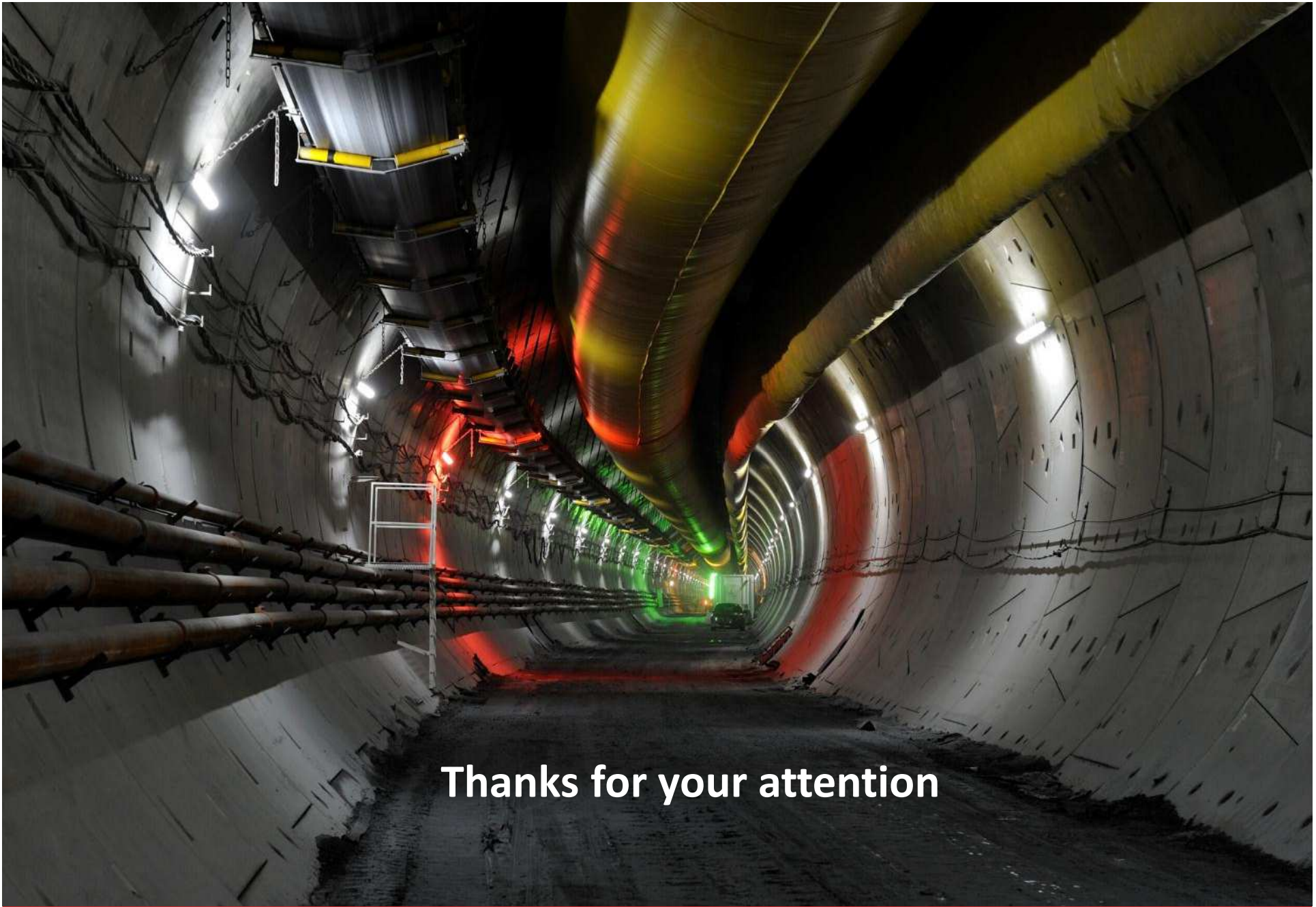
CONCLUSIONS

SYSTRA

CONCLUSIONS

TBM tunnel successfully finished

- A project developed in a well-known geological context, but with a « **new** » **construction method** in this challenging environment, taking advantage of the knowledge acquired on the first tunnel
- Importance of the quality of the **design of the TBM single shield** *suited for high deformable rocks, and asymmetric deformation,*
- Importance of the **quality of the follow up during construction** in order to anticipate and to be reactive:
 - Skilled team
 - Calibration of threshold values
 - Iterative procedure : need to a continuous link between design studies and works
- An average excavation speed of **400m/month**



Thanks for your attention