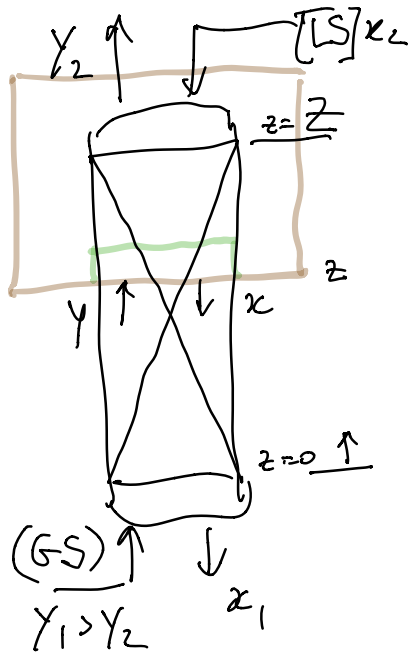


$$N = K_G (y - y^*) = k_G (y - mx)$$

2-film theory $\left[\frac{\text{mol}}{\text{m}^2 \text{s}} \right]$



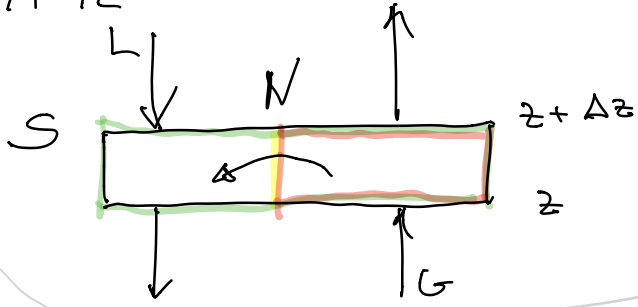
① $Gy + Lx_2 = Gy_2 + Lx$

② $y^* = mx$

③ mass transfer

steady state

(superficial fluxes)
 $G, L, N \left[\frac{\text{mol}}{\text{m}^2 \text{s}} \right]$



specific surface

③ $G S y(z) = G S y(z + \Delta z) + N a \underbrace{S \Delta z}_{\text{volume}}$

or $\left[\frac{\text{m}^2}{\text{m}^3} \right]$ interface area / volume of packing

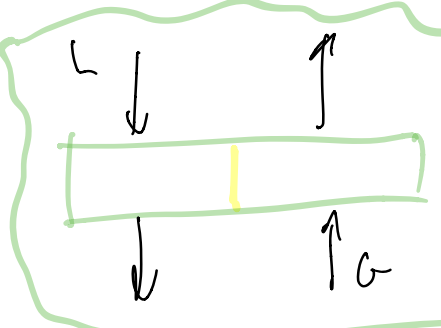
$$\left\{ -a K_G (y - y^*) = G \frac{y(z + \Delta z) - y(z)}{\Delta z} \right\} \xrightarrow{\Delta z \rightarrow 0}$$

①

$$-a k_G (y - y^*) = G \frac{dy}{dz}$$

$$dz = - \frac{G}{a k_G} \frac{dy}{y - y^*}$$

$$\textcircled{3} \int_0^Z dz = Z = - \frac{G}{a k_G} \int_{y_1}^{y_2} \frac{dy}{y - y^*} = \underbrace{\left[\frac{G}{a k_G} \right]}_{HTU} \underbrace{\int_{y_1}^{y_2} \frac{dy}{y - y^*}}_{NTU}$$



$$G y(z) + L x(z + \Delta z) = G y(z + \Delta z) + L x(z)$$

$$L \frac{dx}{dz} = G \frac{dy}{dz}$$

$$\textcircled{2} \frac{G}{a k_G} \int_{y_2}^{y_1} \frac{dy}{y - mx} = \frac{G}{a k_G} \int_{x_2}^{x_1} \frac{A dx}{(A-1)y + y_2 - A y_2^*}$$

$A = \frac{L}{Gm}$
 $y_2^* = m x_2$

$$= \underbrace{\left[\frac{G}{a k_G} \right]}_{HTU} \underbrace{\frac{A}{A-1} \ln \frac{1 - \frac{\alpha}{A}}{1 - \alpha}}_{NTU} = Z$$

$$\alpha = \frac{y_1 - y_2}{y_1 - y_2^*}$$

packed columns
tray columns:

$$N = \frac{1}{\ln A} \ln \frac{1 - \alpha/A}{1 - \alpha}$$

$\left(\frac{L}{G}\right)_{min} \Leftrightarrow A_{min}$?
same for tray and packed columns!!

$$Z \xrightarrow{A \rightarrow d_{min}} \infty$$

specs

$$d_{min} = \frac{y_1 - y_2^{max}}{y_1 - y_2^*}$$

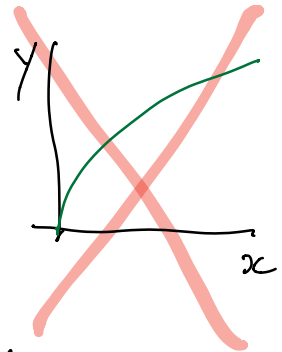
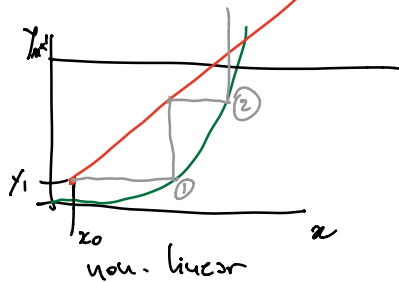
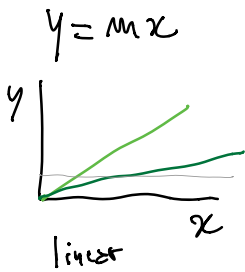
HETP
height
equivalent
theoretical
plates

manufacturers

$$Z = \text{HETP} \times N$$

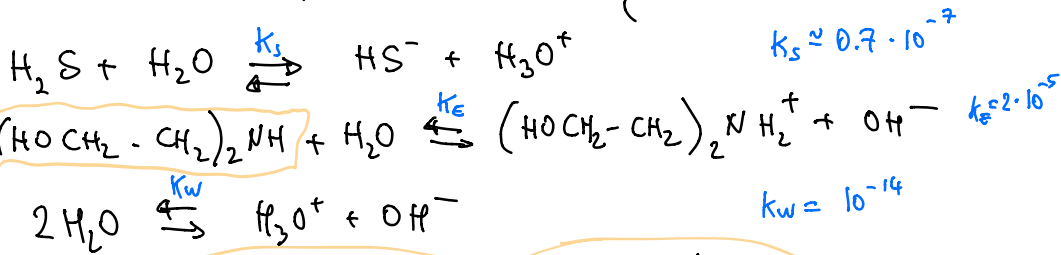
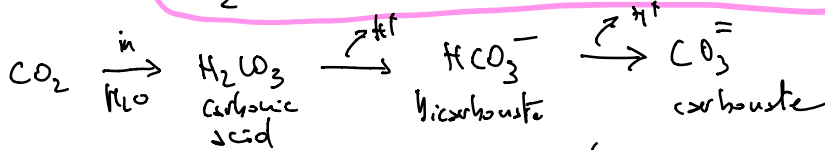
$$\frac{NTU}{m} = \frac{\Delta \ln A}{A-1}$$

physical vs. chemical absorption

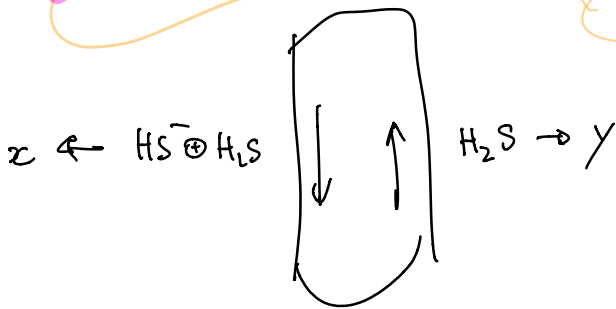


Examples: CO_2 in an aqueous amine solution

H_2S in ν α ν



di-ethanol amine



M.B. x, y

Eq. $y = m x_A$

$x_A < x$

$x_A = f(x)$



B = total sulfur

D = total amine

D & A

(i) $K_s = \frac{SH}{A} \approx 10^{-7}$

(ii) $K_E = \frac{PW}{E} \approx 10^{-5}$

(iii) $K_w = HW \approx 10^{-14}$

(iv) $B = A + S$

(v) $D = E + P$

(vi) $P + H = S + W$

electroneutrality

$A = \frac{H/K_s}{1 + H/K_s} B$ $S = B - A = \frac{1}{1 + H/K_s} B$

$P = \frac{\frac{K_E}{K_w} H}{1 + \frac{K_E}{K_w} H} D$ $E = D - P = \frac{1}{1 + \frac{K_E}{K_w} H} D$

$H + \frac{\frac{K_E}{K_w} H}{1 + \frac{K_E}{K_w} H} = \frac{1}{1 + \frac{H}{K_s}} B + \frac{K_w}{H}$

$pH \approx 10 !! \Rightarrow H = 10^{-10}$

SIMPLIFICATION !!

$1 + \frac{H}{K_s} \approx 1 \Rightarrow S \approx B \Rightarrow A \approx \frac{H}{K_s} B \Rightarrow$ all H_2S is HS^-

$\frac{K_E}{K_w} H \approx 0.1 \Rightarrow 1 + \frac{K_E}{K_w} H \approx 1 \Rightarrow E \approx D \Rightarrow P = \frac{K_E}{K_w} H D$

$P \left(\frac{K_E}{K_w} D + 1 \right) H = \frac{K_w}{H} + B \approx B \Rightarrow P = B$

$W = K_E \frac{D - P}{P} = K_E \frac{D - B}{B} = [OH^-]$

$H = \frac{K_w}{W} = \frac{K_w}{K_E} \frac{B}{D - B} = [H_3O^+]$

$A = \frac{K_w}{K_E K_s} \frac{B^2}{D - B} = [H_2S]$

$x_A = \frac{A}{C_{tot}} = \frac{K_w}{K_E K_s} \frac{B^2/2}{(D - B)/C_{tot}} = \frac{K_w}{K_E K_s} \frac{x^2}{x_D - x}$

solution $C_{tot} ?$
 $x_A = \frac{A}{C_{tot}}$ $x_D = \frac{D}{C_{tot}}$

$x = \frac{B}{C_{tot}}$

$y = m x_A =$
 $= m' \frac{x^2}{x_D - x}$

4

$$m_1' = m \frac{k_w}{k_e k_3}$$

